

resistance of the ground electrode 30 can be enhanced. One end of the core material 38 preferably extends to a portion near the noble metal tip 31, and the other end of the core material 38 preferably extends to the metal shell 50. The coefficient of thermal conductivity of the core material 38 is preferably higher than the coefficients of thermal conductivity of both the ground electrode 30 and the noble metal tip 31. Further, the coefficient of thermal conductivity is preferably increased in the order of the noble metal tip 31, the ground electrode 30, and the core material 38. The core material 38 may be formed of, for example, a copper alloy or pure nickel. The ground electrode 30 having the core material 38 can be produced by, for example, a clad material that has a material forming the core material 38 at the center of the material forming the ground electrode 30, being subjected to plastic processing such as drawing process.

[0036] FIG. 5 illustrates a schematic configuration of an ignition system 200 that includes the spark plug 100. The ignition system 200 is a system for igniting air-fuel mixture supplied to the internal combustion engine. The ignition system 200 includes the spark plug 100, a first power supply 210, and a second power supply 220. The ignition system 200 further includes a control unit 230, an impedance matching circuit 240, and a mixing circuit 250.

[0037] The first power supply 210 is a power supply that applies, as first power, a high voltage for causing spark discharge in the spark plug 100, between the center electrode 20 and the ground electrode 30.

[0038] The second power supply 220 is a power supply that applies, as second power, a voltage having a relatively high frequency (for example, higher than or equal to 1 MHz and not higher than 20 MHz), to the spark plug 100. The second power is applied between the center electrode 20 and the ground electrode 30 by the second power supply 220 while spark discharge is generated.

[0039] The mixing circuit 250 connects the first power supply 210 and the second power supply 220 to the spark plug 100. The mixing circuit 250 includes a coil 251 and a capacitor 252. The coil 251 is connected between the first power supply 210 and the spark plug 100. The capacitor 252 is connected between the second power supply 220 and the spark plug 100. The coil 251 inhibits power from the second power supply 220 from being inputted into the first power supply 210. The capacitor 252 inhibits power from the first power supply 210 from being inputted into the second power supply 220. When the first power supply 210 includes a coil, the coil 251 may not be provided.

[0040] The impedance matching circuit 240 is connected between the second power supply 220 and the mixing circuit 250. The impedance matching circuit 240 matches an output impedance of the second power supply 220 with an input impedance on the mixing circuit 250 and the spark plug 100 sides (that is, load side) during spark discharge in the gap G. Thus, attenuation of the second power supplied to the spark plug 100 can be inhibited.

[0041] The control unit 230 is a device for controlling a time when power is supplied to the spark plug 100 from each of the first power supply 210 and the second power supply 220. The control unit 230 is formed by, for example, an ECU (Electronic Control Unit) that includes a CPU (Central Processing Unit) and a memory.

[0042] The ignition system 200 having such a structure allows high electric energy to be supplied to the spark plug 100. For example, electric energy of 400 to 500 mJ which is a sum of the first power and the second power can be supplied to the spark plug 100. Therefore, even when the spark plug 100 is mounted to an internal combustion engine in a highly compressed and highly supercharged state, ignitability for air-fuel mixture can be improved.

B. Result of Evaluation Test

B1. Ratio S1/S2 in Area:

[0043] Table 1 indicates test results of an ignitability test and a wear resistance test for various samples (sample Nos. 1 to 30) of the spark plug 100. The test result represents a relative evaluation in comparison with a spark plug (sample No. 0) that was prepared as comparative example. The ground electrodes 30 of the samples including the sample of comparative example were formed of the same material (Inconel (registered trademark) 601). Further, the noble metal tips 31 of the samples including the sample of comparative example were formed of the same material (platinum alloy). In each of the samples indicated in Table 1, the coefficient of thermal conductivity of the ground electrode 30 is lower than the coefficient of thermal conductivity of the noble metal tip 31. In each of the samples including the sample of comparative example, the gap G was 1.1 mm in size. In each of the samples including the sample of comparative example, the ground electrode 30 did not include the core material 38.

TABLE 1

No.	Center electrode (mm)	Tip size (mm)	Ground electrode (mm)	L1 (mm)	L2 (mm)	T (mm)	S1 (mm ²)	S2 (mm ²)	S1/S2	Ignitability	Wear resistance
0	Φ1.2	1.5 × 0.7	2.7	0.65	0.00	0.30	0.79	0.60	1.32	—	—
1	Φ0.8	0.9 × 0.9	2.7	0.10	0.20	0.40	0.40	0.72	0.56	A	A
2	Φ0.8	0.9 × 0.9	2.7	0.20	0.10	0.40	0.47	0.63	0.74	A	B
3	Φ0.8	1.4 × 1.4	2.7	0.10	0.20	0.40	0.40	1.82	0.22	A	A
4	Φ0.8	1.4 × 1.4	2.7	0.20	0.10	0.40	0.47	1.68	0.28	A	A
5	Φ0.8	1.8 × 1.8	2.7	0.10	0.20	0.40	0.40	3.06	0.13	B	A
6	Φ0.8	1.8 × 1.8	2.7	0.20	0.10	0.40	0.47	2.88	0.16	B	A
7	Φ1.1	1.4 × 1.4	2.7	0.10	0.20	0.40	0.83	1.82	0.46	A	A
8	Φ1.1	1.4 × 1.4	2.7	0.10	0.40	0.40	0.64	1.82	0.35	A	A
9	Φ1.1	1.4 × 1.4	2.7	0.30	0.10	0.40	0.91	1.54	0.59	A	A
10	Φ1.1	1.9 × 1.9	2.7	0.10	0.20	0.40	0.83	3.42	0.24	A	A
11	Φ1.1	1.9 × 1.9	2.7	0.30	0.20	0.40	0.83	3.04	0.27	A	A
12	Φ1.1	2.2 × 2.2	2.7	0.10	0.20	0.40	0.83	4.62	0.18	B	A